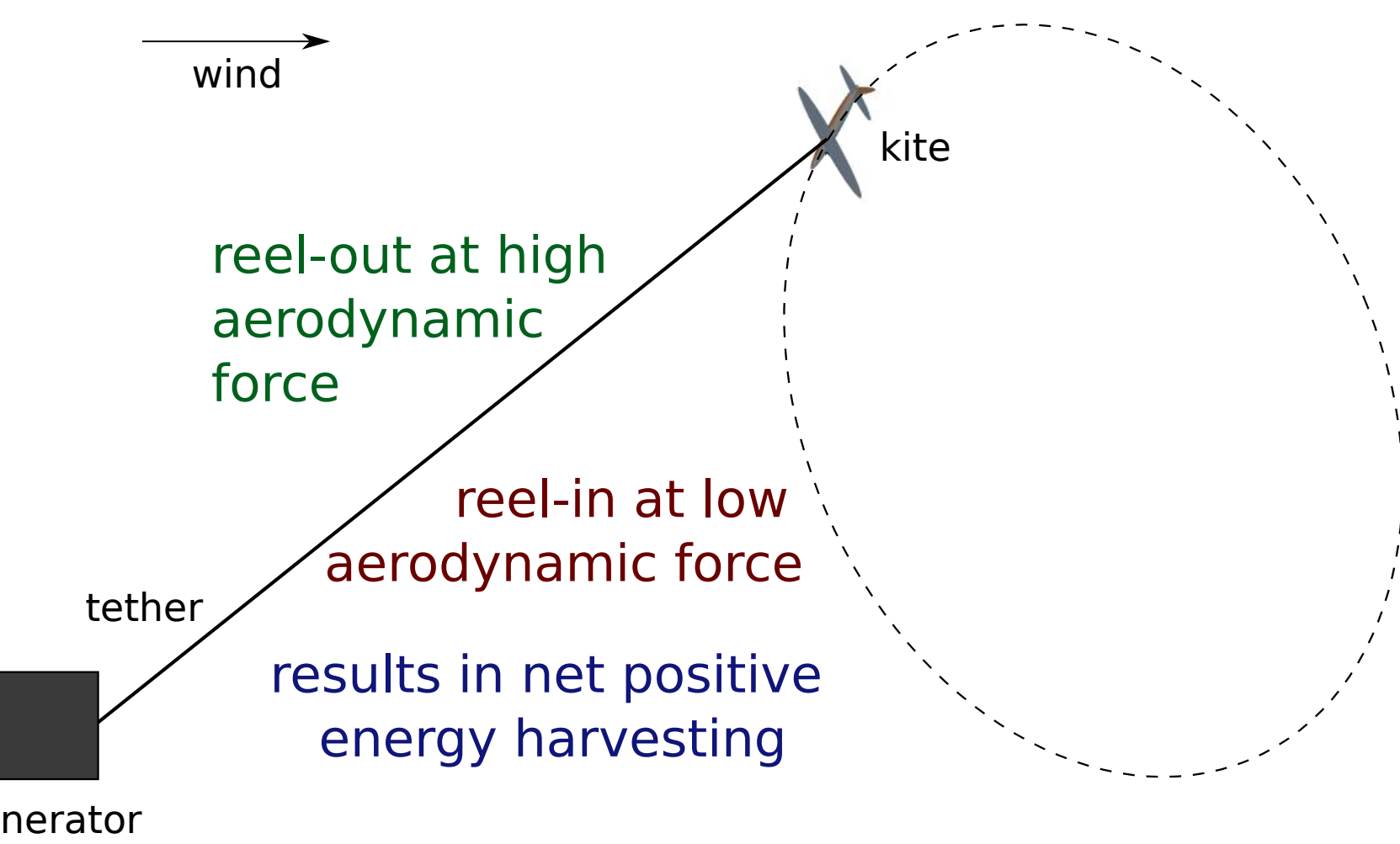


# Rigid-Wake Lifting-Line Vortex Modeling in a Single-Kite AWE Optimal Control Problem

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Airborne Wind Energy (AWE) systems can react quickly to demand or grid requirements.



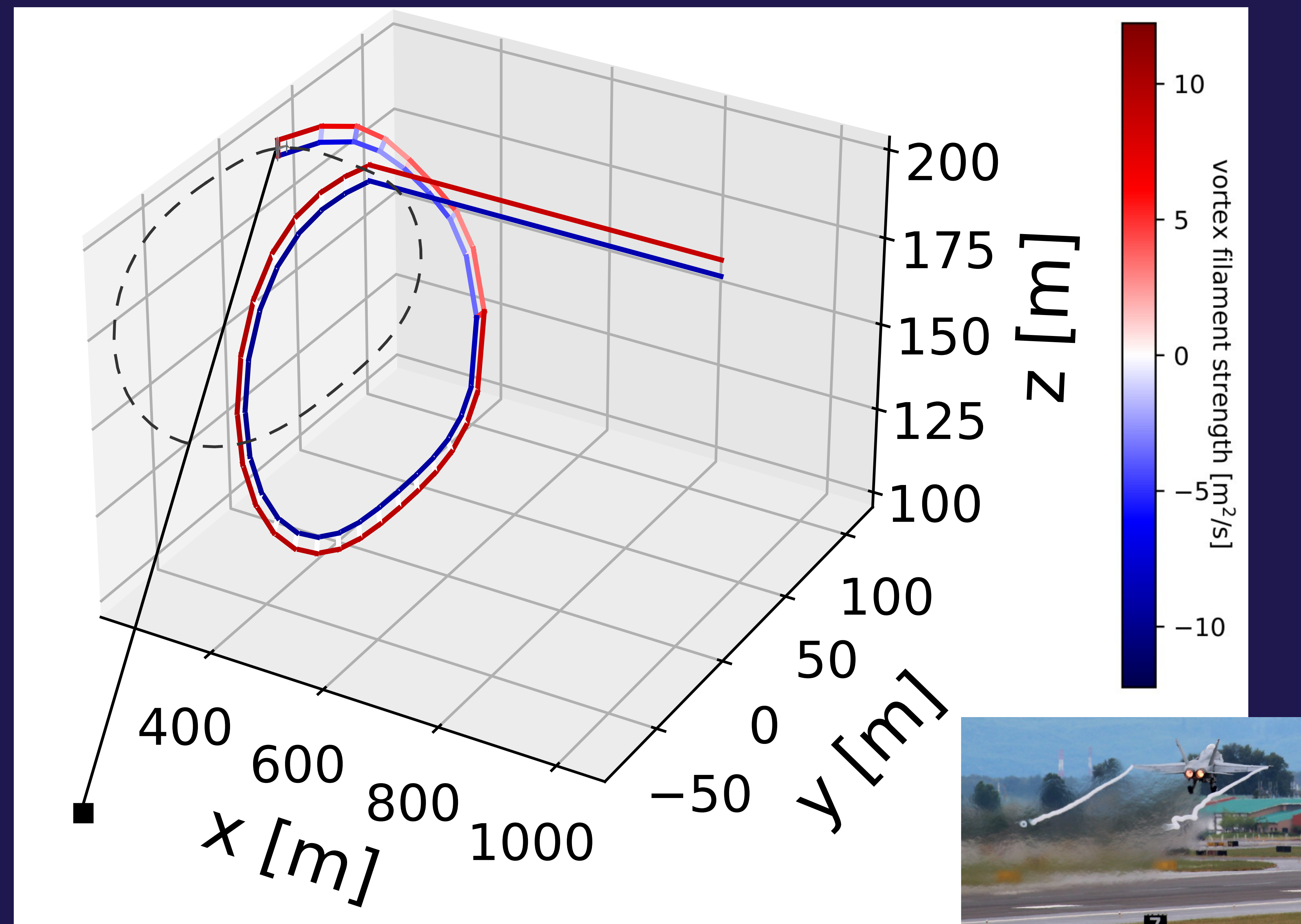
We can predict the system performance - e.g., during initial design phases or financing - by solving Optimal Control Problems (OCP) like

$$\begin{aligned} & \text{minimize} && -\frac{1}{T} \int_0^T \frac{P(t)}{\pi R^2} dt \\ & \text{subject to} && F(\dot{x}(t), x(t), u(t), \theta) = 0, \forall t \in [0, T], \\ & && h(x(t), u(t), \theta) \geq 0, \forall t \in [0, T], \\ & && x(0) - x(T) = 0 \end{aligned}$$

Such a prediction can only be as good as the model used in the OCP, including the model of the momentum transfer in the disturbed flow (the wake). One way to describe fluid's behavior is to model the sources of circular-motion in the flow (vortex).

What happens if we include a rigidly-convected lifting-line vortex model in a single-kite AWE OCP?

# In single-kite airborne wind energy optimal control problems, we only need to include a small amount of fluid history for a good description.



(center) Snapshot of a power-optimal single-kite AWE system, showing the wake modeled with rigidly-convected vortex filaments, shed from the kite's lifting-line. This image shows the case of 30 control intervals, one period of a resolved 'near' wake, and a 'far' wake that conserves circulation. (bottom right) Photo of vortices shed from a plane at take-off. Photographer: Eric Prado



Download the poster



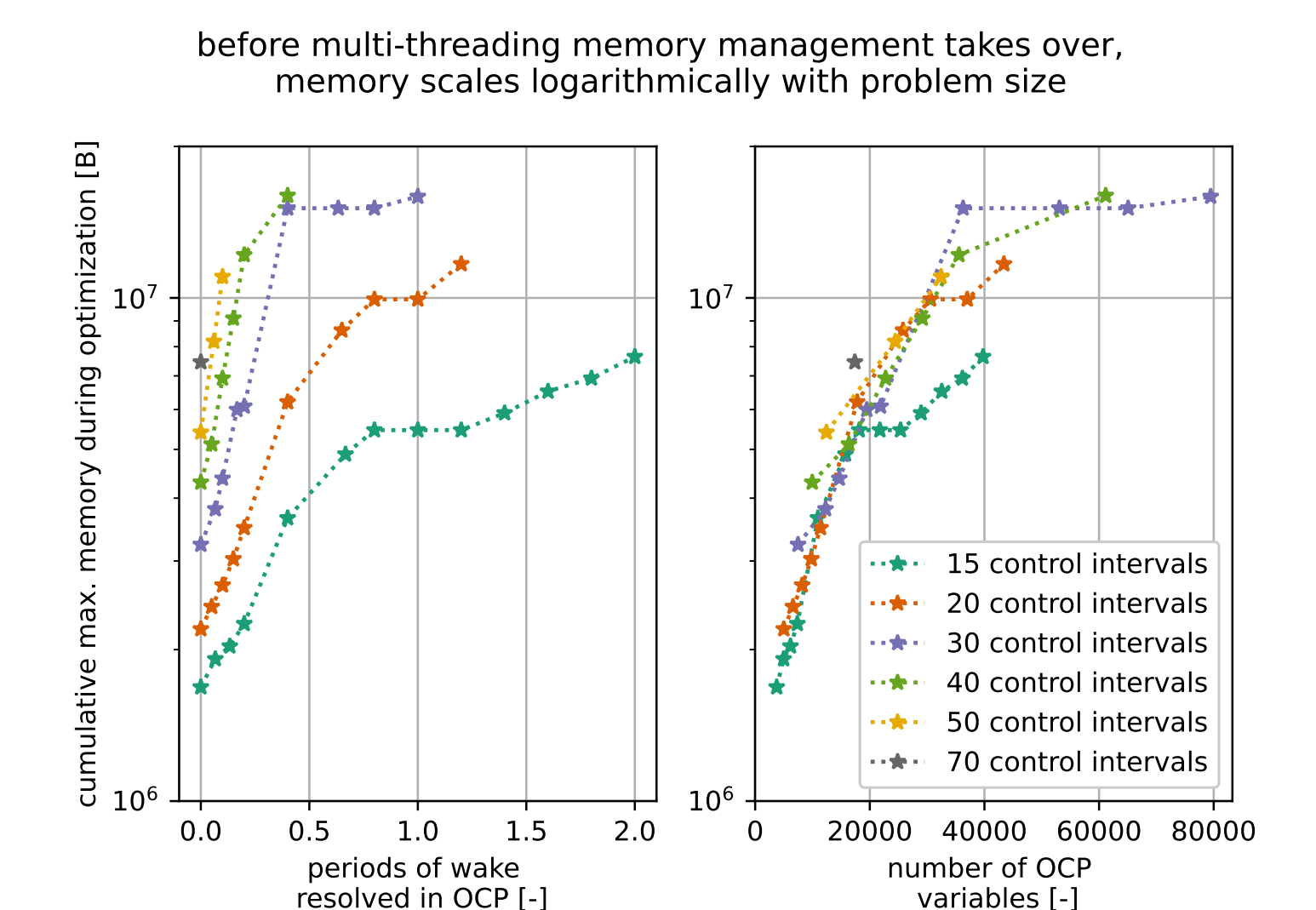
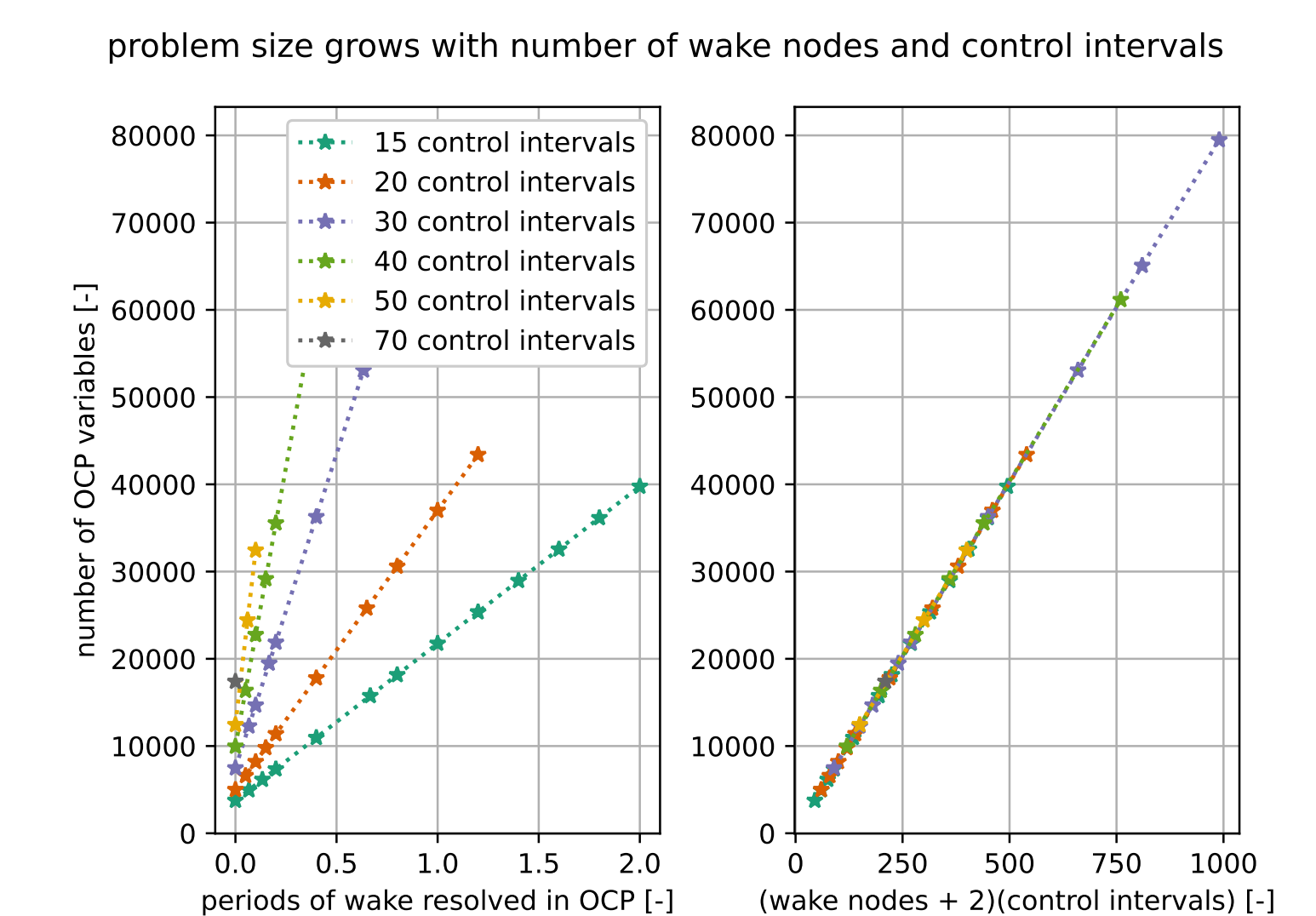
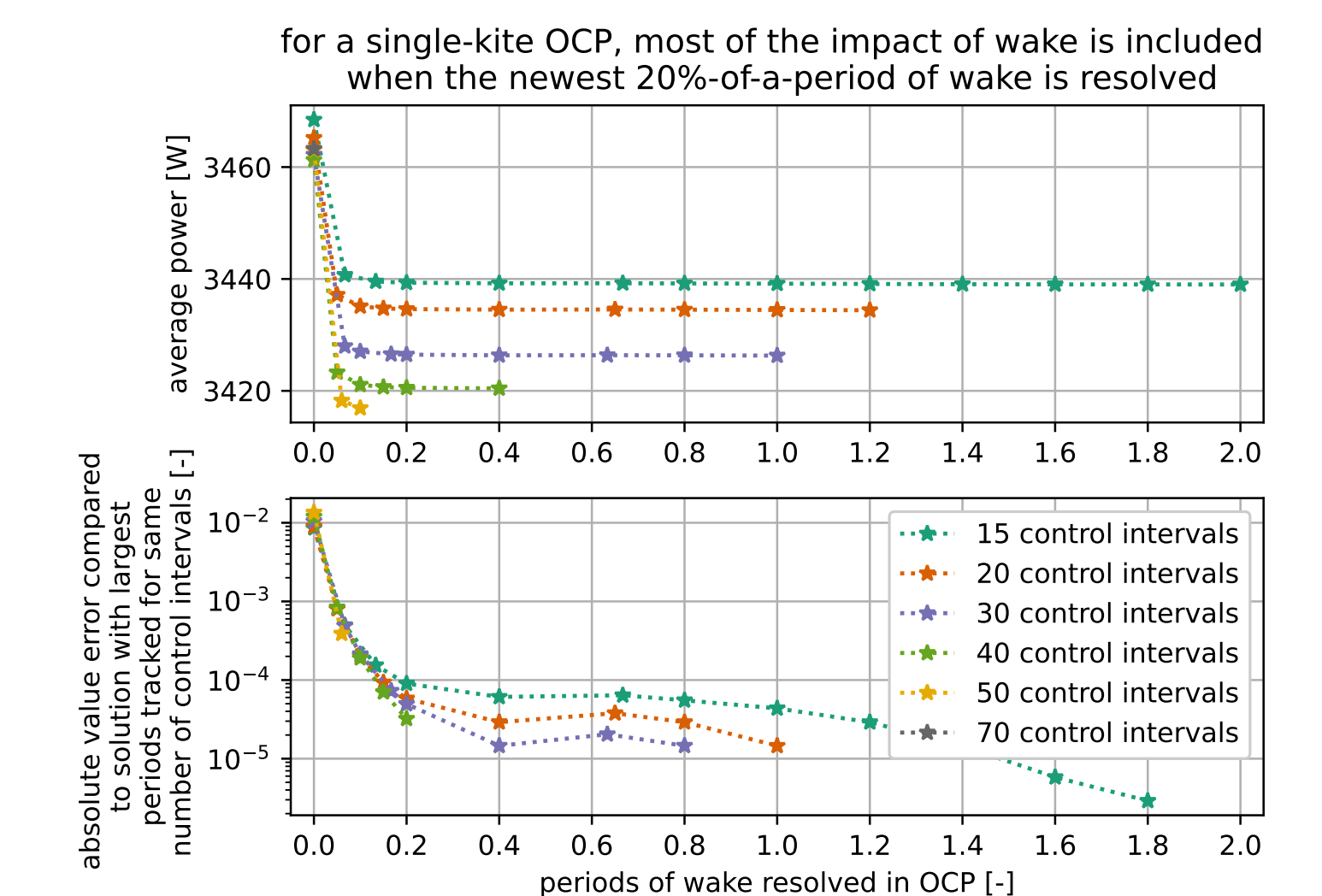
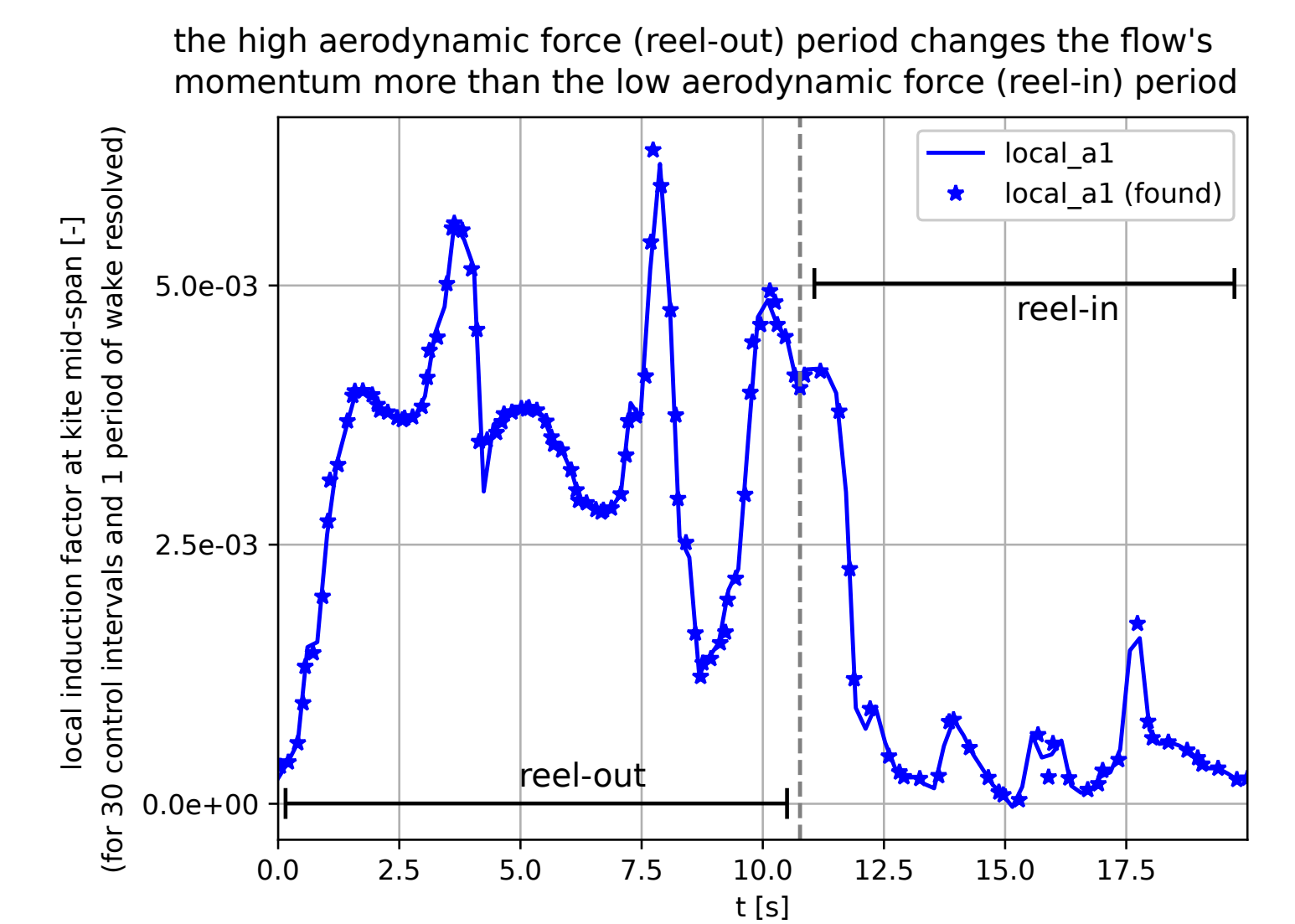
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## Formulate and solve in awebox

**Atmosphere** International Standard Atmosphere  
**Wind** Log Wind Profile with 5m/s wind speed at 10m height  
**Kite** 6 DOF model of the Ampyx AP2, attached at COM, in lift-mode operation  
**Other** time period between 5 and 20s, and fixed tether diameter of 2cm

**Model Constraints**  
 maximum rotational velocity, minimum rotational velocity,  
 maximum tether force, minimum tether force,  
 maximum airspeed, minimum airspeed,  
 maximum angle of attack and sideslip, minimum angle of attack and sideslip.

**OCP** Discretized with Radau direct collocation of order 4, using zero-order-hold controls and single-reelout phase-fixing. One-winding initialization by homotopy.



## Literature

[3] de Schutter, J., et al. (2023). AWEbox: An Optimal Control Framework for Single- and Multi-Aircraft Airborne Wind Energy Systems. Energies, 16(4).